WILSONS MILLS RD.
MUNSON TP.

99

LEVEL BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

Wilson Mills Road - No. 8 - Sec. G.

Benchmarks - pg - 1-2

X-Sections - pg - 3-23

Slope Stakes - pg - 24-45

℄ Profile (1962) at Woodie Brook 46
100

TR 100 ALIGNMENT 1983 - PARTIAL (WOODIEBROOK) 50

99

WILSONS MILLS Rd.
MUNSON TP.

Bench Marks.

B.M. #1.

Spike in N. Root 20" Apple E. Side
Town Line Rd. (165' So of Wilsons Mills Rd)
El. 1014.83

B.M. #2.

Bent Spike in So. Root 22" Maple
31' Lt. (of Rd.) Sta 7+88
El. 1031.745

B.M. #3. Spike in No. Root 36" Walnut
54' Rt. Sta 22+17
Elev. 1085.675

B.M. #4
Spike in No. Root 16" Walnut
22' Rt. Sta 40+20
Elev. 1116.425

B.M. #5
Spike in Top of 20" Stump
22' Lt. Sta 47+08
El. 1161.715

B.M. #6
Spike in No. Root 16" Cherry
31' Rt. Sta 58+25
El. 1221.08

B.M. #7
Bent Spike in No. Root 14" Maple
25' Rt. Sta 71+03
Elev. 1209.505

(1' Ab. Ground)

B.M. #8 Bent Spike in No. Side 16" Locust 36' Rt.
Sta 79+31 El. 1217.59

B.M. #9 Spike in N. Root 18" Ash 19' Rt.
Sta 87+06 El. 1244.25

B.M. #10 ~~Bent~~ Spike in Top of Stump
28' Lt. Sta 92+82
Elev. 1268.235

B.M. #11 Spike in N.W. Side 14" Apple
72' Lt. Sta 100+21
Elev. 1275.35

B.M. #12 Spike in N.E. Root 18" Hickory
30' Rt. Sta 109+35
Elev. 1255.94

B.M. #13 Nail in N.W. Corner Top
Concrete Step Fr. School House
Elev. 1253.965

Wilsons Mills Rd. May 6, 1930 (Fair)

J. Gold Jr
S. Merritt
H. Barton

Sta	+	H.I.	-	Elev	Rem.	South	℄	North
B.M.	5.51	1020.34		1014.83	Spike in N Root 20" Apple 16.5' So of ℄ Rd. (4th tree from [illegible] E Side Town Line Rd. El. 1014.83			
-1+0							10.4	
-0+50							9.5	
0+0						6.6/100 7.3/50 7.2/30 6.9/15 7.6/11	8.5	8.9/7 7.8/9 7.3/20 7.4/30
+30	E. Ditch (Town Line Rd.)					8.8/200 7.8/100 7.5/67 7.3/37 6.9/29 6.7/20 7.3/7	8.1	
1+0						6.2/30 6.3/15 6.8/11	7.1	7.3/4 6.7/6 7.5/15 8.2/30
+12	℄ 12" C.I.P.					6.2/33 5.8/16 8.6/16 8.9/F.L. 6.1/12 6.6/8	6.8	6.7/8 9.1/F.L. 9.8/47 10.3/75 11.9/90
+36	℄ Drive						6.3	6.9/8 7.4/30 7.7/60 (4.8/H.)
2+0						5.9/30 5.5/18 5.2/13 6.1/12 5.6/10	5.3	5.5/7 6.5/9 5.4/11 6.1/17 7.0/30
+30						3.9/30 3.7/18 4.5/14 4.7/12 5.7/10 5.1/8	4.8	5.0/7 6.0/9 4.4/10 5.0/15 6.4/30

Sta	+	H.I.	-	Elev	Rem's
		1020.34			
T.P.	6.56	1022.82	4.08	1016.26	
3+0					
4+0					
T.P.	8.65	1028.51	2.96	1019.86	
5+0					
6+0					
7+0					
T.P.	7.82	1034.19	2.14	1026.37	
B.M.			2.43	1031.76	Bent Spike S. Root 31' Lt. Sta 7+88 El. 1031.745
8+0	Also	Drive			
B.M.	2.43	1034.175		1031.745	
9+0					
T.P.	12.87	1045.39	1.655	1032.52	
10+0					

South — ℄ — North

1.6/30 2.2/19 4.1/13 6.8/10 5.9/8 5.7 6.0/6 7.0/9 6.2/11 8.1/30

3.1/30 3.1/20 3.6/14 5.5/12 4.5/10 4.4 4.7/4 5.1/6 3.0/9 2.1/30

7.0/30 7.3/15 9.2/12 8.4/10 8.4 8.5/4 8.8/6 5.4/10 2.1/30

3.3/30 4.7/21 5.0/15 7.2/13 6.3/10 5.9 6.1/4 7.0/7 4.9/8 3.3/10 3.0/15 1.1/30

2.5/30 2.6/15 4.7/12 3.9/9 3.3 3.4/6 4.7/9 2.5/11 0.3/15 +2.5/30

5.5/30 4.6/14 7.6/11 7.2/8 7.0 6.0/9 7.2/10 (Pitch) 5.5/13 3.9/25 3.4/30

3.8/30 3.6/19 3.6/9 5.5/7 4.2/5 4.1 4.0/10 5.1/12 2.6/15 2.4/30

9.7/30 9.6/19 9.8/12 11.1/8 13.9/5 13.3/4 12.9 12.6/4 13.0/10 14.0/12 11.1/15 11.7/30

May 7, 1930 (Fair)

S. Gold Jr
S. Merritt
H. Barton

Sta	+	H.I.	-	Elev	Rem's	South ... ℄ ... North
		1045.39				
10+75						2.8/30 3.6/17 4.9/12 11.6/7 11.5 11.7/8 12.3/10 8.2/14 10.3/30
11+0						3.4/30 4.5/16 5.8/12 11.3/7 11.0/4 10.9 10.9/9 11.5/10 7.8/14 8.5/18 9.4/30
T.P.	2.15	1042.725	4.815	1040.575		
12+0						2.5/30 2.9/21 4.4/12 7.3/9 6.2/6 5.9 6.2/6 7.0/9 5.3/10 6.9/30
13+0						1.0/30 2.5/18 2.7/12 4.3/11 3.7/9 4.0 4.3/4 4.8/6 4.1/8 5.6/30
14+0						1.3/30 1.1/14 2.2/13 2.1/11 1.5/10 1.5 1.6/4 3.0/6 1.4/8 2.9/30
T.P.	7.95	1049.79	0.885	1041.84		
15+0						5.4/30 5.0/20 5.5/17 7.3/15 6.2/13 6.2 6.2/3 7.1/5 2.9/7 0.9/11 2.0/14 2.4/30
15+60						0.1/30 +0.1/29 +1.2/25 0.0/21 2.7/17 5.3/14 4.5/12 4.2 4.2/2 5.2/4 2.7/6 0.0/10 +8.7/17 +7.6/22 +7.8/30
16+0						+0.7/30 +1.9/25 +2.4/20 0.0/17 1.4/15 4.0/12 3.0/10 2.9 2.8/3 3.5/4 +1.8/8 +7.5/13 +10.2/17 +9.9/30
T.P.	11.51	1060.27	1.03	1048.76		
17+0						7.0/30 6.6/22 5.0/12 9.2/10 7.4/6 7.3 7.0/7 8.2/9 3.2/12 4.0/17 4.8/30
+65						1.0/30 0.6/25 +2.7/16 0.0/12 4.3/9 3.1/7 2.9 2.8/7 3.6/9 +1.0/13 +0.6/15 0.5/18 1.9/30

Sta	+	H.I.	−	Elev.	Rem.
18+0		1060.27			
T.P.	9.59	1069.73	0.13	1060.14	
18+35					
19+0					
T.P.	10.310	1078.87	1.17	1068.56	
20+0					
21+0					
22+0					
T.P.	8.905	1086.98	0.795	1078.075	
B.M.			1.29	1085.69	Spike in N. Root 36" Walnut 54' Rt. Sta 22+17 El. 1085.675
22+40					
23+0					
+47		℄ Drive			

South ℄ North

+5.7/30 +9.5/21 +8.6/18 +3.4/14 2.7/10 1.1/8 1.1 0.9/7 1.9/10 +5.1/16 +3.1/19 +2.1/30

+0.2/30 +0.2/28 +2.4/19 0.0/16 4.9/11 8.4/8 8.4 8.2/5 8.7/8 2.5/14 4.0/20 5.1/30

+5.1/30 +4.4/25 +4.5/17 0.0/12 3.1/8 2.4/7 2.3 2.4/7 2.8/8 +1.5/12 +0.8/18 +0.1/30

+3.9/30 +2.9/22 +2.4/13 0.0/8 6.4/4 5.6/3 5.7 6.1/10 3.5/13 5.4/23 6.9/30 10.5/40

+0.9/30 1.3/8 3.4/5 2.9/4 3.1 3.9/11 5.7/14 8.0/30 10.0/40

+2.4/30 +1.5/16 0.0/10 1.6/9 0.9/7 1.2 1.5/13 2.8/18 4.1/28 5.5/40

(1.2/H) 2.4/30 3.4/22 6.7/11 8.8/8 8.2/5 8.0 8.5/9 4.6/17 4.3/30

6.4/30 5.3/23 5.1/10 6.9/7 6.3/6 6.2 6.5/9 1.2/27 0.9/30 (+1.2/H)

4.6 3.6/10 2.2/30

Sta	+	H.I.	-	Elev	Remi
		1086.98			
23+71		(℄ Drive South)		(℄ Gate North)	
24+0					
24+70					
T.P.	9.12	1095.77	0.33	1086.65	
25+0					
25+79.5 (P.C.)					
26+0					
T.P.	10.31	1105.87	0.21	1095.56	
26+50					
26+77.89 (P.T.)					
27+0					
27+27.89 (P.C.)					

South ℄ North

4.8/√0 4.3/30 4.7/F.L.(8') 4.0/8 4.0 3.8/9 4.2/F.L.(9') 3.4/27 3.5/30

3.6/30 3.8/27 2.6/10 3.7/8 3.4/6 3.2 3.1/7 3.8/9 2.2/11 2.7/26 2.9/30

+2.8/30 +3.5/17 +2.0/15 +0.6/10 1.3/9 0.6/7 0.3 0.4/5 1.8/8 0.1/10 +1.1/12 +0.9/21 +1.0/25 +1.0/30

+0.5/30 +0.8/22 3.1/18 6.4/12 8.8/10 7.8/8 7.8 7.9/√ 9.0/7 6.6/9 2.6/15 2.5/18 3.1/21 2.3/25 2.8/30

+10.4/30 +9.4/27 +8.8/24 4.0/13 3.5/12 3.3 3.5/2 3.9/4 +2.9/7 +2.6/10 +0.9/21 1.4/30

+11.9/30 +9.8/24 2.8/13 2.1/12 1.8 2.1/2 +3.1/5 +1.8/12 0.0/17 0.2/20 2.8/30

+5.1/30 +5.0/28 +2.8/23 9.0/12 8.5/11 8.3 8.5/2 2.3/7 4.0/13 5.7/18 5.8/20 8.4/30

+6.2/30 +5.9/25 +3.6/22 6.5/11 5.8/9 6.1 6.1/2 6.7/3 3.6/6 5.1/14 6.7/19 9.8/30

+4.1/25 +1.4/20 +0.5/16 1.9/12 4.9/10 4.1/8 4.4 4.7/3 5.1/5 4.6/6 7.3/10 9.8/25 11.3/30
+5.0/30

+3.2/30 +1.8/22 0.8/18 2.1/13 3.0/10 4.1/8 3.1/6 3.3 3.8/8 8.1/21 8.7/27 9.2/30

May 8 '30

1105.87

Sta	+	H.I.	−	El.	Rem's
T.P.	7.61	1110.15	3.33	1102.54	
27+50					
27+75					
28+0					
T.P.	5.79	1114.77	1.17	1108.98	
28+50					
29+0					
T.P.	11.37	1125.17	0.97	1113.80	
30+0					
T.R.	9.25	1133.04	1.38	1123.79	
31+0					
31+45					
T.P.	8.03	1140.37	0.70	1132.34	
32+0					

(Fair)

S. Gold Jr.
S. Merritt
H. Barton

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South ℄ North

1.4/30 3.1/21 6.4/16 6.9/8 7.8/7 6.8/5 6.9 7.5/10 9.5/14 10.8/20 11.5/28 11.6/30

0.7/30 2.3/20 6.0/15 6.4/7 7.1/6 6.2/5 6.1 6.5/9 7.0/12 6.2/13 6.7/16 9.2/25 9.7/30

0.3/30 1.1/24 3.0/18 5.1/11 5.7/6 6.4/5 5.7/3 5.4 5.2/4 5.5/11 6.1/12 6.1/14 5.6/15 6.4/20 7.2/25 7.2/30

3.4/30 3.2/21 4.2/13 8.6/6 9.6/4 8.4/2 8.3 8.6/11 9.2/13 7.2/14 5.5/18 7.5/25 9.0/30

4.6/30 3.4/22 2.5/10 6.9/6 5.9/3 6.0 6.4/8 6.9/10 5.1/13 9.3/30

1.5/30 1.9/18 2.6/12 9.9/5 9.6/4 9.4 9.6/8 10.8/10 5.9/16 5.8/20 7.1/30

0.2/30 +0.2/24 0.2/18 0.2/15 8.1/8 7.5/7 7.2 7.6/5 8.2/6 1.9/11 3.5/25 3.7/30

+0.7/30 +1.8/21 +2.5/15 4.0/8 4.0 4.5/6 +6.0/16 +6.0/22 +5.5/24 +5.7/30

4.9/30 4.5/21 3.9/13 7.3/10 6.8/8 6.4 6.7/4 7.2/5 3.8/8 4.1/18 4.6/23 4.3/26 4.3/30

Sta	+	H.I.	−	Elev.	Rem's
32+55		1140.37			
33+0					
33+65					
T.P.	0.585	1130.255	10.70	1129.67	
34+0					
35+0					
35+33.40	(P.C.)				
T.P.	4.36	1127.87	6.745	1123.51	
35+65	W. Bank of Gravel Pit				
35+75					
36+0					
36+25					

South ℄ North

2.6/30 1.9/23 1.7/15 2.4/12 5.0/10 4.5/9 3.7/2 3.9 4.5/5 5.6/8 4.1/9 2.6/14 2.9/19 3.7/23 3.5/26 4.1/30

5.9/30 4.4/22 4.3/18 3.8/9 6.7/8 5.8/6 5.4/4 5.8 6.1/3 6.5/4 2.3/8 1.5/10 2.3/25 3.9/30

15.4/30 11.5/17 9.7/14 11.1/12 10.3/5 10.6 10.7/1 11.2/3 7.2/6 1.4/13 1.7/26 2.1/30

6.8/30 6.5/27 4.0/21 3.7/18 2.1/13 2.5/12 2.9/10 2.9 3.2/2 3.5/3 1.5/4 +4.4/17 +5.1/22 +5.5/30

11.5/30 9.5/27 8.4/18 6.0/13 5.9 6.1/2 7.0/4 6.0/5 5.0/13 4.6/20 3.1/22 3.1/30

14.3/30 13.3/25 12.1/20 6.5/14 6.1/7 6.5/1 6.9 7.7/2 6.5/3 5.3/8 5.4/15 5.0/17 5.1/23 6.0/30

10.6/30 7.9/24 4.4/16 4.2/7 4.8 5.2/1 3.3/3 0.1/7 0.1/12 0.8/21 2.5/30

9.4/30 6.6/24 4.8/20 4.4/7 4.9 5.3/1 4.5/3 4.1/10 3.0/17 10.3/27 10.5/30

9.4/30 6.7/21 4.8/16 4.5/7 5.0 5.3/3 5.1/5 5.0/9 7.4/19 8.2/27 8.3/30

12.1/30 11.1/28 9.6/22 7.3/18 5.2/13 4.8/5 5.1 5.5/3 5.1/7 5.2/19 1.1/30 +3.2/37 Top Bank

Sta	+	H.I.	−	Elev.	Rem's
36+50		1127.87			
36+75					
37+0					
T.P.	3.32	1122.28	8.91	1118.96	
37+16.92	P.T.				
38+0					
T.P.	5.885	1121.395	6.77	1115.51	
39+0					
40+0					
B.M.			4.98	1116.415	Spike in N. Root 16" Walnut 22' Rt. Sta 40+20 El. 1116.425
40+37	℄	Drive			
T.P.	7.65	1126.41	2.635	1118.76	
41+0					
41+60		℄ Drive			

South ℄ North

14.0/30 11.5/22 10.5/18 5.6/11 5.1/4 5.2 5.6/4 5.2/10 +1.1/18 +1.9/22 +4.1/28 +3.7/30

12.4/30 9.1/20 5.4/12 5.2/10 6.6/9 6.0 6.3/4 6.8/6 4.5/8 1.2/13 0.0/21 +0.1/30

11.8/30 6.0/20 4.6/16 4.6/12 5.6/9 8.3/7 8.2 8.9/3 9.3/5 5.2/11 5.6/18 5.2/24 6.2/30

13.3/30 10.1/25 1.4/14 0.8/11 1.3/9 3.8/7 3.5 4.2/7 1.8/10 1.8/17 2.1/19 1.4/23 2.7/30

16.0/30 14.5/27 6.6/15 6.0/8 6.3/7 5.8/6 5.7 6.5/13 7.4/15 7.1/16 8.0/23 9.6/30

6.1/30 5.3/13 5.2/7 5.6/6 5.1/4 5.1 6.1/13 6.8/15 6.9/22 8.8/28 8.7/30

5.4/30 3.9 3.9/30

7.9/30 5.6/18 3.4/4 3.3

9.2/30 8.1/20 7.5/14 7.0/10 6.8 7.0/11 7.9/19 8.2/30 (8.7/44)

5.3 5.8/30 6.2/50

May 9, 30

Sta	+	H.I. 1126.41	−	Elev.	Rem's
42+0					
T.P.	12.72	1137.42	1.71	1124.70	
42+68	℄	12" Corr. I. Pipe (Hillside)			
42+77	℄	Drive			
43+0					
T.P.	5.28	1141.76	0.94	1136.48	
44+0					
T.P.	11.00	1152.67	0.09	1141.67	
45+0					
T.P.	11.53	1163.93	0.27	1152.40	
46+0					
47+0					
B.M.			2.20	1161.71	Spike Top of 20" stump. 22' Lt Sta 47+08 El. 1161.715

(Fair)

S. Gold Jr
S. Merritt
H Barton

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South ℄ North

3.9/30 3.2/21 3.2/15 4.7/13 4.1/11 3.9 4.0/8 4.4/10 2.7/11 1.8/30

8.6/30 8.7/21 12.2 F.L. 11.1/15.7 10.5/14 10.8/11 10.1 9.6/4.7' 10.3 F.L. 7.8/7 0.6/23 0.2/30

8.2/30 9.9 F.L. 8.5/14 8.7

(21/H) 4.1/30 3.4/24 4.2/18 8.1/14 7.7/12 7.7 7.7/3 8.3/4 +1.9/18 +3.4/24 +4.1/30

+0.1/30 0.1/21 0.5/12 3.6/9 3.3/6 2.9 2.9/8 3.4/9 2.7/11 +0.7/17 +1.9/30

+0.3/30 0.5/20 1.5/11 7.4/6 7.0/5 6.6 6.8/9 7.3/11 3.5/15 3.0/18 4.2/30

0.6/30 7.9/13 10.8/4 10.3/3 10.7 10.0/4 10.4/10 11.2/12 8.1/15 8.5/18 10.1/23 11.5/30

+4.0/30 +1.9/17 1.7/10 3.2/8 2.8/6 2.7 2.9/8 3.8/10 2.1/12 4.3/18 6.1/30

Sta	+	H.I.	-	Elev.	Rem's
B.M.	8.315	1170.03		1161.715	
47+68					
48+0					
48+50					
49+0					
T.P.	7.035	1172.825	4.24	1165.79	
49+92	℄	2½ x 3½	Stone	Culvert	
50+0					
50+25.10	P.C.				
50+50					
50+75					
T.P.	11.865	1182.465	2.225	1170.60	

South ℄ North

+7.9/30 +6.9/25 1.8/13 4.4/9 3.8/7 3.4 3.8/7 4.8/10 0.5/15 +0.4/18 +0.3/20 0.5/24 1.5/30

+6.4/30 +4.7/22 1.3/13 3.6/11 3.6/10 2.7/8 7.6 2.8/8 4.2/11 2.7/13 0.0/18 0.7/30

+1.1/30 1.4/17 5.1/12 4.9/10 3.7/8 3.8 4.3/10 5.3/12 4.3/13 4.8/17 6.3/27 6.8/30

7.0/30 3.2/22 4.3/14 5.3/13 5.1/11 4.2/9 4.2 4.6/7 5.1/9 4.8/10 5.1/13 7.1/17 9.1/30

10.9/19 11.6/F.L. 6.1/14.5 6.2/13 7.4/13 7.4/9 6.9/7 6.0 5.8/5 6.9/10 7.1/12 7.1/14 12.4/T.F.L. 14.3/F.L. 18.6/27

7.6/100 9.9/31 10.1/27

8.9/30 7.9/26 10.0/21 10.3/14 8.5/9 5.9/6 5.7 5.6/7 14.5/21 15.6/30 16.8/38 12.8/45

8.8/30 7.7/23 6.3/7 5.6/4 5.3 4.9/7 6.3/12 11.2/25 9.3/30

7.3/30 5.7/16 4.3/11 5.0/9 4.9/8 4.1/7 4.1 4.0/8 3.8/10 3.4/13 4.8/16 3.7/19 4.0/23 0.8/30

5.6/30 4.4/21 2.8/16 2.3/12 2.7/11 3.6/10 2.2/5 2.6 2.2/10 2.9/12 2.9/14 1.8/16 +4.3/28 +4.6/30

Sta	+	H.I.	−	Elev.	Rem³
51+0		1182.465			
51+35.29	P.T.				
52+0					
T.P.	13.115	1194.545	1.035	1181.43	
52+75					
53+0					
53+25					
T.P.	11.04	1204.66	.925	1193.62	
54+0					
54+28	℄	Drive North			
55+0					
55+09	℄	Drive South			

South ℄ North

6.7/30 6.4/19 8.9/13 11.6/11 10.4/6 10.4 10.5/9 11.2/12 9.0/16 2.8/28 2.5/30

3.7/30 3.4/27 3.3/21 3.1/17 8.7/12 7.5/8 7.6 7.8/8 9.1/11 5.6/14 +0.6/26 +0.8/30

+5.2/30 +5.5/26 +5.2/22 +5.6/20 +5.7/18 2.6/11 1.5/10 1.1 0.9/7 3.0/10 +6.8/22 +8.2/30

0.5/30 +0.2/24 +0.6/20 7.6/11 6.3/8 6.4 6.8/5 8.0/6 7.9/8 4.9/12 4.1/15 +2.8/30

1.0/30 +0.1/25 +0.7/19 5.3/12 4.4/9 4.0 4.2/5 5.3/7 2.6/10 0.1/30

2.8/30 1.9/26 1.2/18 4.2/13 3.0/11 2.4 2.4/4 3.5/6 0.0/12 +1.5/15 +1.5/28 +4.1/33

5.6/30 6.1/28 6.4/16 7.8/15 8.0/13 9.3/12 7.8/9 7.4 6.8/10 7.1/14 6.9/16 6.4/30

1.4/30 3.8/16 6.8/11 7.9/10 6.6/8 6.1 6.0/9 6.4/13 5.8/26 5.7/30 (6.6 F.L. Pipe)

+3.5/30 +2.4/21 0.0/16 1.5/10 2.1 2.7/9 3.2/12 0.0/15 +1.3/24 +2.5/30

(+7.9/H.) +3.9/75 +1.7/30 0.0/10 1.6

May 10 '30

Sta	+	H.I. 1204.66	−	Elev.	Rem's
T.P.	10.665	1215.31	0.015	1204.645	
56+0					
56+54.65 (P.C.)					
T.P.	7.455	1221.575	1.19	1214.12 1221.08 (Used)	
B.M.	2.61	1223.69	0.49	1221.085	Spike in N. Root 16" Cherry 31' Rt. Sta 58+25 El. 1221.08
56+75					
57+0					
57+25					
57+50					
57+75					
58+0					
58+25					

(Fair)

S. Gold Jr
S. Merritt
H. Barton

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South					℄				North
3.5/30	4.3/21	5.4/15	7.5/11	6.5/8	6.4	6.5/7	7.7/10	5.5/12	5.0/30
3.1/30	4.1/11	5.1/8	4.3/4	4.0		4.5/9	5.4/12	4.3/14	3.8/30
11.0/30	11.9/9	13.0/7	12.2/4	11.7		12.0/10	13.1/13	11.9/15	11.1/30
9.6/30	10.9/8	12.1/5	11.1/3	10.8		11.0/11	12.0/14	10.9/16	9.5/30
8.3/30	10.1/7	11.1/4	10.5/3	10.2		10.0/11	11.2/14	9.6/17	8.1/30
6.8/30	7.5/16	9.0/6	10.0/5	9.3/2	9.2		9.2/12	10.1/15	8.7/16	6.8/30
	5.6/30	7.3/6	9.0/4	8.3/2	8.2		8.3/12	9.1/15	7.6/17	6.6/30
	4.1/30	6.0/7	7.6/5	6.8/2	6.7		6.7/11	7.7/14	5.8/16	5.8/30
	3.1/30	4.8/11	4.5/7	5.7/4	5.4		5.5/10	6.4/13	5.2/15	5.2/27	5.6/30

Sta	+	H.I.	−	Elev.	Rem's
58+58.8	(B.T.)	1223.69			
59+0					
60+0					
60+19	℄	Drive	South		
61+0					
T.P.	1.38	1216.07	9.00	1214.69	
62+0					
63+0					
64+0					
65+0					
T.P.	2.76	1208.93	9.90	1206.17	
66+0					

South ℄ North

3.3/30 3.2/22 4.5/11 5.7/9 4.8/6 4.3 5.0/9 5.6/11 4.7/13 5.3/25 5.8/30

3.5/30 4.9/13 5.9/12 4.7/8 4.6 5.1/9 5.8/11 5.4/12 6.7/30

2.8/H 4.4/30 4.4/19 5.3/11 6.3/9 5.6/7 5.4 5.8/8 6.9/11 6.0/13 6.5/24 7.3/30

5.2/30 5.0/19 6.6/FL→8 6.1/8 6.2

7.8/30 8.4/11 10.1/8 9.2/6 8.9 9.2/11 10.2/14 8.9/16 6.9/25 6.8/30

3.8/30 3.6/13 3.9/8 5.2/6 4.4/4 4.2 4.5/12 5.3/15 4.1/17 2.8/29 2.8/30

6.1/30 6.2/12 6.5/9 7.4/7 6.4/4 6.2 6.6/13 7.4/15 6.5/16 5.8/27 6.0/30

6.9/30 7.6/14 8.2/9 9.5/7 8.0/4 8.0 8.4/12 9.2/13 8.4/15 8.5/30

8.5/30 9.2/13 10.0/9 11.0/8 9.9/5 9.6 10.1/12 11.0/13 10.0/15 9.8/30

3.2/30 3.4/16 3.9/10 5.6/8 4.2/5 4.1 4.4/11 5.4/14 4.5/16 3.8/30

Sta	+	H.I.	−	Elev.	Rem's
67+0		1208.93			
67+17	℄	Drive (North)			
67+75					
68+0					
68+63	℄	2½'×3' Stone culvert			
T.P.	5.09	1205.17	8.85	1200.08	
69+0					
69+40					
T.P.	9.42	1211.48	3.11	1202.06	
70+0					
70+20	℄	Drive South			
B.M.			1.95	1209.53	Bent Spike N. Root 4" Maple 25' Rt Sta 71+03 El. 1209.505
71+0					

South ℄ North

4.9/30 5.0/16 5.5/12 7.8/9 7.0/5 6.5 6.7/10 6.1/12 6.5/15 5.6/17 5.2/22 4.7/30

7.0 7.0/14 8.0/F.L. 5.8/30

8.7/30 8.4/26 8.1/17 8.8/11 9.4/10 8.5/7 8.0 8.4/9 9.0/11 8.6/13 7.1/21 6.6/26 6.1/30 (2.2/H)

10.0/30 9.6/25 9.1/11 9.5/9 8.6/7 8.3 9.1/10 9.2/24 9.0/30

11.4/60 13.3/32 13.7/18 14.1/F.L. 8.6/8.5 8.6/6.5 9.3/6.5 9.0 9.1/11 8.5/11 8.5/13 14.3/F.L. 14.0/28 14.7/58 15.0/88 15.3/118 16.6/220 18.8/250

6.7/30 6.7/30 6.3/23 6.2/19 7.5/16 5.5/12 5.0/3 5.0 5.1/12 6.8/17 7.6/27 8.0/28 8.3/30

0.8/30 1.3/25 2.7/10 4.3/6 5.6/5 5.8/1 5.6 4.7/9 5.1/16 5.6/17 4.9/18 4.1/24 3.8/27 4.3/30

(3.6/H) 5.1/30 6.7/9 9.4/6 9.7/3 8.8 9.4/3 9.3/15 10.1/17 8.6/18 5.7/26 5.9/30

4.0/30 6.3/18 8.1/F.L. 6.8/9 7.8

2.4/30 3.7/11 5.0/9 4.5/6 4.1 3.9/6 4.2/11 5.3/16 4.1/16 3.9/20 4.2/30

Sta	+	H.I.	−	Elev.	Remks
T.P.&B.M.	3.915	1213.42		1209.505	
72+0					
72+63					6" Tile across the field on So. Side 35' off ℄
73+0					
74+0					
T.P.	5.55	1216.78	2.19	1211.23	
75+0					
76+0					
76+02	℄	16" C.I.P. Culvert			
77+0					
77+25					
T.P.	5.36	1218.94	3.20	1213.58	

South ℄ North

4.0/30 5.1/10 6.0/8 5.3/6 5.1 5.7/11 6.3/12 5.3/14 5.2/25 5.6/30

6.2/35' F.L. Tile 7.2/F.L. 5.3/8 4.7 4.6/3 5.5/9 8.0/10 8.7/26 11.0/50

4.0/30 4.6/9 5.3/7 4.7/5 4.5 4.9/8 5.4/11 4.8/17 5.8/25 7.3/30

1.8/36 2.7/9 4.2/8 3.4/6 2.8 2.6/2 3.2/10 4.0/12 3.0/14 2.8/22 2.9/30

3.6/30 4.6/12 5.1/9 5.8/8 4.9/5 4.7 4.8/10 6.3/14 5.4/15 5.0/23 5.4/30

4.4/30 5.3/9 5.8/8 4.6/5 4.8 5.1/10 5.9/12 5.8/14 5.9/20 6.5/30

4.4/30 5.1/10 6.1/F.L. 4.7/6 4.8 5.0/8 6.1/10 7.5/F.L. 6.4/20 7.0/30 8.7/60 11.8/100

2.7/30 2.6/20 3.6/16 3.6/11 4.2/8 4.0 4.1/7 4.8/11 4.2/12 3.0/17 3.5/27 3.1/30

2.6/30 2.3/27 1.8/23 2.8/14 3.3/12 4.3/10 3.9/8 3.7 3.9/6 4.6/8 3.7/9 2.5/15 2.3/30

S. Gold Jr.
J. Merritt } Cloudy
H. Barton

May 12 30

Sta	+	H.I.	-	Elev.	Rem's	South — ℄ — North
77+50		1218.94				2.9/30 2.9/25 5.3/14 6.4/12 5.9/10 5.4/2 5.5 5.6/6 6.7/7 5.4/9 4.0/15 4.2/30
77+75						2.7/30 3.0/25 5.5/14 6.2/13 5.4/11 5.0 5.0/3 6.2/7 5.2/8 3.5/15 3.8/30
78+0						2.6/30 4.5/22 5.2/14 5.8/13 4.9/10 4.8 5.1/4 5.9/6 5.1/7 4.6/14 6.9/22 9.7/30
78+24.90 P.T.						2.2/30 4.9/20 4.7/15 5.0/11 4.2/3 4.5 5.2/5 7.6/12 10.9/17 11.7/30
78+32	℄	24" Cor. I. Pipe				5.4/50 7.7/30 6.8/23 7.7/F.L. 5.6/16.3 4.4/16 4.5 5.4/7 6.3/7.7 8.4/F.L. 9.0/8 9.6/15 11.8/21 14.0/28 15.0/39 15.8/47
79+0						4.2/30 3.3/23 3.1/13 4.0/12 4.0/11 3.2/10 2.6/3 2.7 2.8/5 3.3/7 2.5/8 2.8/12 0.6/19 0.3/30
B.M.	4.13	1221.74	1.33	1217.61	Bent [illegible] N. Side 16" Locust 1' Ab. Grd. 36' Rt. Sta 79+31 El. 1217.59	
79+40						1.3/27 1.4/24 1.5/30 3.8/19 4.1/17 4.9/14 5.8/13 4.9/10 4.4/3 4.4 4.6/4 5.5/7 4.4/8 1.4/15 1.3/21 1.5/30
T.P.	6.74	1226.39	2.09	1219.65		
80+0						2.2/30 2.4/24 7.1/15 8.7/14 7.3/11 7.0 7.0/2 7.9/4 5.4/7 3.3/13 2.9/25 3.5/30
T.P.	10.02	1234.47	1.94	1224.45		
81+0						6.5/25 6.1/30 7.7/21 10.7/18 12.0/16 10.7/15 10.3/11 10.0/5 10.3 10.4/3 10.9/4 7.7/9 7.6/30
81+64	℄	Gate South				3.3/4.4 6.2/30 8.1/25 8.8/19 7.7/15 6.7/4 7.1

Sta	+	H.I.	−	Elev.	Rem's
82+0		1234.47			
83+0					
T.P.	8.99	1242.31	1.15	1233.32	
84+0					
85+0					
86+0					
T.P.	7.38	1249.06	0.63	1241.68	
87+0					
B.M.	4.82	1249.06	4.82	1244.24	Spike N. Root 18" Ash 19' E+. Sta 87+06 El. 1244.25
87+40	℄	Drive South			
88+0					
T.P.	12.72	1260.02	1.76	1247.30	
89+0					
90+0					

South ℄ North

2.8/30 2.9/28 6.7/19 6.5/15 6.0/13 5.6/4 5.9 6.4/3 6.9/6 5.5/7 4.0/9 4.7/30

0.3/30 0.8/23 0.8/19 4.1/16 3.1/13 2.5/4 2.9 3.3/5 3.9/6 2.1/8 2.2/30

5.3/30 5.7/22 7.9/17 7.8/15 8.1/12 7.9 8.3/4 9.2/7 7.2/10 7.4/30

4.9/30 5.2/25 5.6/15 6.6/14 5.5/10 5.5 5.8/5 6.3/6 5.5/7 5.7/10 6.4/11 7.0/30

3.2/30 3.5/23 3.1/11 3.9/10 3.6/8 3.4 3.7/7 4.5/9 3.1/10 3.8/15 4.7/30

4.9/30 5.5/20 6.4/16 6.5/12 7.0/9 8.4/8 7.5/6 7.3 7.3/8 8.4/11 7.1/12 6.8/14 6.9/30

3.6/30 7.0 5.5/8 F.L. → 6.0

0.7/30 1.2/19 2.3/10 2.6/8 4.0/7 3.1/5 3.0 3.1/8 4.3/11 3.2/12 1.8/16 2.4/20 2.1/23 2.1/30

8.3/30 8.5/23 9.5/14 10.5/8 11.5/7 10.8/5 10.7 11.2/9 11.7/11 10.0/13 9.8/16 10.4/21 10.5/30

0.5/30 0.7/27 1.6/17 2.9/12 3.8/8 6.3/6 5.9/5 5.7 6.0/7 6.5/10 7.1/12 4.7/14 2.9/17 3.0/30

Sta	+	H.I. 1260.02	−	Elev. Rems
T.P.	12.95	1272.405	0.565	1259.455
90+83	℄ Drive South			
91+0				
91+30				
91+75	℄	12" Tile		
92+0				
B.M.			4.175	1268.23
93+0				
B.M.	7.22	1275.455		1268.235
94+0				
95+0				
96+0				

Spike in Top of 15" Hump Lt. 28' Sta 92-82 El. 1268.235

South	℄	North
(4.8 H) 10.2/34 11.5/20 13.8/FL→14 14.2		
8.9/30 9.7/28 10.7/18 11.1/15 13.3/11 13.0/9 13.2	13.4/7 13.8/9 11.7/11 13.3/24 14.0/30	
10.1/30 11.2/24 12.2/15 13.0/14 12.4/12 12.3	12.5/6 11.8/7 12.5/11 14.9/21 15.6/30	
12.0/31 12.5/24 12.9/17 13.4/FL→14.3 11.3/13 11.4	11.3/2 12.3/3.7 14.0/FL. 15.0/30 15.6/50 17.8/72	
10.2/30 10.8/19 12.0/17 11.1/15 10.5/12 10.7	10.5/5 11.3/9 11.0/13 11.5/25 11.6/30	
2.0/30 2.7/26 5.8/19 8.1/15 6.5/11 6.3	6.5/3 7.3/5 4.1/9 4.1/17 4.6/30 (5.4 H)	
3.6/30 3.6/27 5.1/20 5.9/14 6.7/13 6.1/9 5.7	5.9/7 6.9/9 5.8/10 6.0/21 6.3/30	
3.1/30 4.1/22 4.7/14 5.6/12 4.7/10 4.3	4.8/8 5.6/10 4.8/11 5.0/30	
2.1/30 3.0/19 3.6/13 4.6/12 3.9/10 3.2	3.5/8 4.7/10 3.5/11 3.0/21 2.6/26 2.8/30	

Sta	+	H.I.	−	Elev.	Rem's
97+0		1275.45			
T.P.	6.37	1279.59	2.235	1273.22	
98+0					
99+0					
100+0					
B.M.			4.23	127536	Spike in NW side 14" Appig 72' Left Sta 100+21 El. 1275.35
101+0					
101+62		℄ Drive North			
102+0					
T.P.	3.00	1275.62	6.97	1272.62	
103+0					
104+0					
T.P.			6.82	1268.80	

South ℄ North

1.3/30 2.3/21 2.7/13 3.1/12 2.8/10 2.1 2.6/6 3.5/10 3.2/12 3.4/30

4.8/30 5.8/14 6.9/13 6.1/10 5.3/7 5.0 5.9/10 6.9/12 6.1/13 6.2/30

4.3/30 4.5/23 5.1/14 6.1/13 5.1/10 4.6 5.2/9 6.0/11 5.4/12 5.9/30

3.0/30 3.4/20 4.8/18 5.9/11 4.7/9 4.3 4.8/9 5.4/11 4.8/12 4.5/30

3.2/30 3.5/23 3.3/20 3.2/17 4.0/16 5.9/14 4.8/12 4.1 5.2/7 5.7/8 4.8/9 4.0/20 3.8/30 (2.4/H)

6.2 6.3/5 7.1/7 6.8/11 6.0/30

5.4/30 5.9/24 7.0/18 8.1/16 7.3/13 7.1 7.5/5 7.9/6 6.6/7 5.6/13 6.1/30

4.4/30 5.1/19 5.7/17 4.8/15 4.6 4.7/3 5.7/5 5.1/7 5.4/21 5.7/25 6.0/30

5.2/30 5.8/19 7.0/17 5.9/14 5.7 6.1/3 6.9/5 6.2/6 5.8/17 5.9/23 6.4/25 6.1/30

May 13' 30

S. Gold Sr
S Merritt
H Barton

Sta	+	H.I.	-	Elev.	Rem's	South — ℄ — North
T.P.	3.50	1272.30		1268.80		
105+0						3.0/30 3.4/23 4.0/18 4.9/16 4.3/14 4.1 4.4/5 5.1/7 4.3/8 4.3/19 4.0/20 4.1/24 4.4/25 4.5/30
106+0						4.3/30 4.9/22 5.5/14 7.3/12 6.3/10 5.9 6.6/7 7.1/8 5.7/10 5.3/17 4.8/20 4.8/25 5.3/26 5.0/30
107+0						5.8/30 5.9/21 6.3/15 7.6/11 10.2/8 9.6/7 9.0 9.6/8 9.8/9 7.5/11 7.1/12 7.1/30
107+70						7.9/30 7.6/24 8.4/15 10.3/10 12.2/8 11.2/6 10.7 10.7/3 11.3/10 12.0/12 9.3/15 8.9/30
108+0						(9.6/H) 9.3/30 9.4/23 9.9/15 11.6/9 13.1/8 12.4/6 12.3 12.6/10 13.8/13 11.8/14 10.3/17 10.3/25 10.5/28 10.1/30
T.P.	1.82	1261.51	12.61	1259.69		
109+0						2.9/30 2.8/26 3.5/17 5.5/9 7.1/7 6.4/5 6.2 6.6/11 7.2/12 5.0/14 4.2/16 3.9/30
109+17	℄ Drive South					5.6/30 7.8/F.L.→ 6.7/6 7.0
110+0						8.7/30 8.8/23 9.5/14 10.3/10 11.3/8 10.5/7 10.2 10.5/10 11.2/11 9.2/13 8.5/15 8.0/22 7.2/30
B.M.	0.54	1256.48	5.55	1255.94 Used 1255.96	Spike in N.E. Root 18" Hickory 30' Rt Sta 109+35 El. 1255.94	
111+0						7.3/30 7.5/22 7.8/13 8.6/12 7.6/8 7.5 7.8/8 8.3/10 7.7/11 7.3/18 6.9/30

Sta	+	H.I.	-	Elev.	Rem'ks	South	℄	North
112+0		1256.48				10.4/30 9.9/20 9.3/14 9.5/12 8.7/8	8.4	8.8/9 9.2/11 9.1/13 9.8/30
112+85	℄ (18"x6") Stone Culvert					10.9/50 10.8/30 10.8/F.L. 7.6/11 7.6/9 9.4/9 8.8/7	8.5	8.7/8 7.6/8 7.6/9.5' 10.6/F.L. 10.5/16 10.2/30 10.6/45
						11.4/110 12.0/150 12.4/250 13.8/350 15.2/450 17.6/550 21.0 (F.L. 6" Tile - 650' T.B. 18.5'		10.3/75 9.2/100
T.P.	3.11	1251.98	7.61	1248.87				
113+0						5.7/30 5.9/28 5.6/11 5.5/9 4.9/8	4.3	4.7/8 5.3/10 5.9/11 5.3/12 5.5/17 6.0/30
114+0						3.7/26 4.7/21 5.0/17 4.8/14 5.4/13 4.9/12 4.7/8	4.6	4.8/9 5.1/10 4.8/12 4.9/20 5.5/30
						3.6/30		
115+0						1.7/30 2.0/25 3.6/23 3.3/21 3.3/16	3.4	3.4/4 4.7/7 3.4/9 2.7/13 1.7/30
T.P.	8.06	1256.73	3.31	1248.67				
115+45	W. Ditch of N & S. Rd. - 880' to a 2½x3' Stone Culvert					8.8/200 7.5/100 7.2/70 7.1/50 7.0/27 7.3/13	6.9	6.9/16 6.6/20 6.3/30 6.4/40 7.6/40 7.9/44 7.2/47
						14.7/500 11.8/400 10.2/300		7.0/72 7.0/100 7.3/200
115+57.92	℄ N & S. Rd.					7.1/200 6.1/100 6.0/79 6.6/53 6.5/30 6.9/18	6.7	6.5/12 5.4/40 5.4/100 5.9/200
+50							4.6	
+100							4.5	
+140							4.1	
B.M.	-		2.77	1253.96	B.M. Nail in N.W. corner Top Conc. Stop [illegible] El. 1258.[illegible]			

Wilson's Mills Rd. Munson T.P. Aug 7. 1930

Temp 85°+?

S. Gold Jr
S. Merritt
H. Barton

Sta	+	H.I.	-	Elev.	Rem's	South	℄ Elevation	North
B.M.	3.69	1018.52		1014.83				
0+0							1011.80	
1+0						C.0.5 / 22.7'	1014.00	F.1.5 / 20.5
T.P.	4.91	1019.40	4.03	1014.49				
2+0						F.1.0 / 20.3'	1016.20	F.2.0 / 19.7'
T.P.	10.91	1026.10	4.21	1015.19				
2+30						GR / 22.5	1016.86	F.2.0 / 20.1'
3+0						C.3.0 / 26.5'	1018.40	F.3.0 / 19.3'
4+0						F.0.5 / 21.1'	1020.60	F.0.5' / 21.7'
5+0						F.1.5 / 20.3'	1022.80	C.3.5 / 26.7'
T.P.	12.27	1033.56	4.81	1021.29				
6+0						F.1.0 / 20.5'	1025.0	C.2.0 / 24.5
7+0						F.1.0 / 20.7'	1027.20	C.3.5 / 27.0'
B.M.			1.79	1031.77				

Sta	+	H.I.	-	Elev.	Rem's
		1033.56			
8+0					
B.M.			1.79	1031.77	
9+0					
T.P.	10.84	1042.44	1.96	1031.60	
10+0					
+50					
11+0					
+50					
T.P.	9.40	1045.81	6.03	1036.41	
12+0					
+50					
T.P.	10.72	1048.845	7.685	1038.125	
13+0					
+50					
14+0					
T.P.	12.09	1059.585	1.35	1047.495	
15+0					
+59.86					
16+0					
T.P.	6.535	1063.93	2.19	1057.395	

South	Elevation		North
G.R. 22.3'	1029.40		C.1.0 23.1'
F.1.0 21.0'	1031.60		G.R. 22.3'
C.2.0 25.3'	1033.80		G.R. 22.7
C.5.5 30.9'	1034.90		G.R. 22.5'
C.6.0 31.7'	1035.91		C.0.5 23.5'
C.4.5 28.7'	1036.75	F.0.5 22.0'	
C.2.0 25.7'	1037.50		F.1.0 21.1'
	1038.41		
C.1.5 23.9'	1039.63		F.1.5 20.1'
	1041.16		
F.1.5 19.9'	1043.00		F.2.5 19.3'
F.2.0 18.9'	1047.00		C.0.5 23.5'
C.0.5 23.9'	1049.40	C.8.0 35.0'	
G.R. 23.3'	1051.00		C.9.0 35.5'

Sta	+	1063.93 H.I	−	Elev	Rem's
T.P.	12.87	1072.05	4.75	1059.18	
17+0					
+65					
18+0					
T.P.	7.12	1077.62	1.55	1070.50	
19+0					
T.P.	12.57	1086.84	3.35	1074.27	
20+0				1085.675	
B.M.	0.95	1086.625	1.10	1085.74	
21+0					
T.P	1.035	1080.73 1083.245	6.93	1079.695	
22+0					
T.P.	10.205	1090.10	3.34	1079.895	
22+40					
B.M.			4.43	1085.67	
23+0					
T.P.	8.66	1090.88	7.88	1082.22	
24+0					

South	℄ Elevation	North
F. 2.0 / 20.5'	1055.75	C. 0.5 / 22.9'
C. 1.0 / 24.7	1059.68	F. 0.5 / 22.0
C. 4.0 / 29.7'	1062.00	C. 1.5 / 24.7'
C. 6.0 / 31.1'	1069.00	C. 1.5 / 24.7'
C. 8.0 / 32.0	1075.40	F. 1.5 / 21.0
C. 1.5 / 24.1'	1078.20	F. 7.0 / 28.5
F. 0.5 / 23.0'	1080.40	F. 5.0 / 23.3'
C. 3.0 / 26.0'	1081.28	C. 2.0 / 25.3'
F. 1.0 / 21.1'	1082.60	C. 3.0 / 26.5'
F. 2.0 / 19.9'	1085.475	F. 1.0 / 21.1'

Sta	+	H.I.	−	Elev	Remarks
		1090.88			
24+70					
T.P.	12.16	1100.28	2.76	1088.12	
25+0					
T.P.	11.15	1110.39	1.04	1099.24	
+79.5		Slope 1¼:1 So. Side			
26+0		Slope 1¼:1 So. Side			
T.P.	8.07	1116.20		1108.13	
+25		→ slope < than 1½:1 (So Side)			
26+50		same			
+77.89		same			
27+0					
T.P.	3.86	1112.21	7.85	1108.35	
+25					
T.P.	5.71	1108.66	9.26	1102.95	
+50		1½:1 Slope North Side (Emb)			
T.P.	2.58	1105.66	5.58	1103.08	
+75					

South		℄ Elevation		North
F.0.5 / 22.6		1090.12		F.2.0' / 20.3'
C.3.5 / 28.3		1092.40		C.0.5 / 22.7
C.8.0 / 32.0		1098.29		F.2.0 / 20.0'
C.8.5 / 32.0'		1099.63		F.4.5 / 23.5'
(+25)	C.8.0 / 32.0	1101.06		F.4.5 / 23.0
C.8.5 / 32.0		1102.30		F.2.0 / 19.0'
	C.8.5 / 32.0	1103.43		F.7.5 / 27.5'
C.6.5 / 32.0	1104.38		1104.08	F.9.5 / 31.0'
C.3.0 / 26.0'	1105.36		1104.76	F.7.0 / 32.0
C.1.5 / 23.7'	1106.15		1105.25	F.6.5 / 32.0'
C.1.5 / 23.3'	1106.95		1105.75	F.5.0 / 31.5

Sta	+	H.I.	−	Elev.	Rem's
T.P.	5.38	1113.83		1108.45	
28+0					
+25					
28+50					
+75					
29+0					
T.P.	7.35	1118.73	2.45	1111.38	
+25					
+50	7' Berm on N. Side				
T.P.	12.67	1129.23	2.17	1116.56	
30+0					
T.P.	11.64	1139.425	1.445	1127.785	
31+0					
+60	Slope < than 1½:1 (N. Side)				

South		℄ Elevation		North
C. 0.5 / 20.5'	1107.65		1106.45	F 3.5 / 30.3'
C. 1.5 / 24.0	1108.56		1107.36	F 0.5 / 31.5'
C. 2.0 / 24.7	1109.67		1108.47	F 2.0 / 29.5'
GL / 22.7'	1110.67		1109.77	F 5.5 / 31.5
F. 0.5 / 21.5'	1111.88		1111.28	F 6.0 / 30.3'
	1113.30		1113.00	
	C. 1.5 / 25.5'	1115.06	F 3.0 / 20.5	
	C. 4.0 / 28.5'	1119.49	F 0.5 / 22.0	
	C. 4.5 / 29.3'	1128.54	C. 1.0 / 24.5	
C. 2.5 / 27.0		1131.48		C. 6.5 / 32.0

Sta	+	H.I.	-	Elev	Left
		1139.425			
32+0					
	5.28	1140.95	3.755	1135.67	
+50					
33+0					
T.P.	8.95	1141.82	8.08	1132.87	
+65	7' Berm South Side				
T.P.	0.72	1133.595		1132.87	
34+0					
T.P.	5.61	1038.48	0.72	1032.87	
+50	Emb. Slope < than 2:1 (So Side)				
T.P.	3.82	1029.52	12.78	1025.70	
35+0					
T.P.	2.43	1129.21		1126.78	
+33.40	Emb. Slope 1½:1 So Side				
T.P.	1.57	1120.12		1118.55	
+58.40	Emb. Slope 1½:1 So Side				

South		℄ Elevation		North
	C. 2.5 27.0	1133.17		C. 3.0 27.0'
	C. 4.5 29.1'	1133.60		C. 3.5 27.1'
	C. 1.5 26.0'	1133.18		C. 4.0 28.9'
	F. 4.0 22.3'	1131.69		C. 6.0 32.0
	F. 7.0 29.5'	1130.98		C. 4.5 29.5'
	F. 11.5 32.0	1129.20		C. 3.0 26.5'
F. 8.5 32.0	1127.05		1127.78	F. 0.5 20.5'
F. 10.0 32.0	1125.71		1126.38	F. 1.0 20.5'
F. 8.0 32.0	1124.71		1125.72	GS 23.5'

Sta	+	H.I.	−	Elev.	Remks
		1129.21			
35+75					
36+00					
T.P.	11.20	1134.09	6.32	1122.89	
+25	Slope < than 2:1 South Side				
+50	Slope Less than 2 :1 (South Side)				
T.P.					
+75	(Stake to be Checked)				
T.P.	3.14	1126.09		1122.95	
37+00	(7' Berm on So. Side)				
+16.92					
L 41.92					
38+00					
T.P.	6.12	1120.92	11.29	1114.80	
38+50					

South		℄ Elevation		North
F. 2.5 / 23.5'	1124.05		1125.29	F. 3.5 / 20.0'
F. 3.5 / 27.3'	1123.05		1124.39	F. 4.5 / 24.3'
F. 6.5 / 32.0	1122.05		1123.39	F. 0.5 / 20.5'
F. 8.0 / 32.0	1121.05		1122.39	C. 9.5 / 32.0
F. 5.0 / 27.0'	1120.05		1121.28	C. 6.0 / 31.5'
F. 1.0 / 27.5'	1119.05		1119.95	C. 3.0 / 25.5'
F. 1.5 / 19.5	1118.42		1119.09	C. 2.0 / 24.1
	1117.58		1117.92	
F 3.0 / 19.0		1116.30		F. 1.5 / 20.3'
		1115.68		

Sta	+	H.I.	−	Elev.	Remarks
		1120.90			
39+00			4.50	1116.40	
B.M.	5.97	1122.395		1116.425	
+50					
40+00					
+50					
B.M.	7.95	1124.375		1116.425	
41+00					
41+50	Special Ditch on N. Side				
T.P.	8.65	1130.405	1.60	1121.755	
42+00					
T.P.	9.74	1134.08		1124.34	
+68	Slope > than 1½:1				
T.P.	8.70	1142.70		1134.00	
43+00	Slope < than 1½:1				

South	℄ Elevation	North
Gr. 22.7'	1115.60	F. 1.0 20.7'
C. 2.0 25.0	1116.08	C. 0.5 22.7'
F. 0.5 21.5'	1117.10	C. 0.5 23.0
F. 2.0 20.5	1118.40	F. 0.5 21.3'
F. 1.5 20.1'	1120.04	F. 1.0 20.3'
F. 1.0 20.5	1122.35	F. 2.0 21.0
F. 2.0 19.3'	1122.34	F. 1.0 20.5'
F. 1.5 20.5	1130.44	C. 5.5 32.0'
C. 1.0 23.3	1133.00	C. 9.0 32.0

Sta	+	H.I.	-	Elev	Cen's
		1142.7v			
44+0					
T.P.	4.87	1146.87	.7v	1142.00	
45+0					
T.P.	11.80	1153.80	4.87	1142.00	
46+0					
T.P.	1v.36	1165.36	0.80	1153.00	
+50					
T.P.	7.09	1171.09	1.36	1164.00	
47+00					
B.M.			9.345	1161.745	
+50	Slope < than 1½:1				
T.P.	10.45	1177.85	3.69	1167.40	
48+00	Slope < than 1½:1				
T.P.	6.30	1182.40	1.75	1176.10	
+50	7' Berm N. Side				
T.P.	0.80	1177.90	5.30	1172.10	
49+00	7' Berm N. Side				
T.P.					

South & Elevation North

South	Elevation	North
C. 1.0 / 23.5'	1141.00	C. 2.5 / 25.7'
C. 4.0 / 28.0	1149.00	Gr. / 23.0'
C. 7.0 / 32.0	1157.00	F. 2.0 / 20.0
C. 6.0 / 30.5'	1161.00	F. 3.5 / 21.3'
C. 3.0 / 25.7'	1164.40	F. 5.5 / 25.3'
C. 9.5 / 32.0	1166.60	C. 0.5' / 23.3
C. 9.5 / 3v.0	1167.60	C. 2.0 / 25.7'
C. 3.5 / 26.5'	1167.40	F. 2.5 / 19.5
Gr. / 22.3	1167.04	F. 5.5 / 25.0

Sta	+	H.I.	-	Elev.	Remks.
		1177.90			
49+50	Slope < than 2:1		N. Side	7' Berm	
T.P.	6.14	1171.29	11.75	1066.15	
50+0					
+25					
+50					
T.P.	11.87	1181.83	2.33	1169.96	
+75					
51+0	Slope	1 3/4 : 1	N. Side		
T.P.	11.71	1191.11	2.43	1179.40	
+35.29	Slope	< than	1 1/2 : 1		
51+50	Slope	< than	1 1/2 : 1		
52+0	Slope > than 1 1/2 : 1 South Side				
	Slope < than 1 1/2 : 1 North Side				

South		℄ Elevation		North
F. 1.5 / 19.0		1167.65		F. 14.5 / 32.0
F. 1.0 / 28.5	1169.04		1168.89	
F. 5.5 / 27.0	1170.22		1169.92	F. 7.0 / 31.1
F. 5.5 / 27.3'	1171.61		1171.16	F. 0.5 / 23.3
F. 5.0 / 27.5'	1173.23		1172.63	C. 5.5 / 32.0
C. 1.0 / 24.3'	1174.83		1174.32	C. 6.5 / 32.0'
C. 2.0 / 24.9'	1177.40		1177.10	C. 6.5 / 32.0
C. 2.0 / 25.0'	1178.56		1178.35	C. 7.0 / 32.0
C. 3.0 / 29.0'		1183.00		C. 7.5 / 32.0

Sta	+	H. I. 1191.11	−	Elev.	Remks
T.P.	12.81	1198.81	5.11	1186.00	
52+50	Slope	< than	1½:1	N. Side	
+ 75					
53+0					
T.P.	8.90	1203.87	3.84	1194.97	
+50					
T.P.	11.92	1212.73	3.06	1200.81	
54+0					
+28					
+50					
55+0					
+50					
56+0					
B.M.	0.67	1211.75		1211.08	
+54.65					

South	℄ Elevation		North
C. 4.5 / 29.5'	1187.50		C. 8.0 / 32.0
	1189.63		
C. 2.5 / 27.0	1191.75		C. 2.0 / 25.0
	1193.63		
F. 1.5 / 21.0	1195.50		C. 2.0 / 25.3
F. 0.5 / 21.5'	1199.00		F. 1.0 / 20.9'
	1200.85		
C. 3.0 / 25.9'	1202.31		F. 1.5 / 19.9'
C. 2.5 / 25.7'	1205.25		C. 0.5' / 23.0'
C. 2.5' / 25.3	1207.81		C. 1.5 / 24.3'
C. 1.5 / 24.3'	1210.00		C. 1.0 / 23.1'
F. 0.5 / 20.9'	1212.41	1211.85	GS / 23.9'

Sta	+	H.I	-	Elev	Remarks
		1v21.75			
56+99.65					
57+04.65					
+75					
+50					
+25					
58+00					
+17.85					
+25.85					
B.M.	3.24	1v24.32		1v21.08	
59+00					

South		℄ Elevation		North
F.1.0 / 20.1'	1v13.54		1v12.66	Gr. / 25.3
F.0.5 / 18.7	1v14.51		1v13.40	C.1.0 / 27.5'
Gr. / 21.1'	1v15.05		1v13.94	C.1.5 / 28.7'
C.1.0 / 22.9'	1v15.65		1v14.54	C.2.5 / 29.7'
C.2.0 / 23.7'	1v16.17		1v15.06	C.2.0 / 29.0'
C.2.5 / 25.1'	1v16.67		1v15.56	C.2.5 / 30.5'
C.3.5 / 24.7'	1v16.77		1v15.93	C.2.5 / 29.7'
C.4.0 / 27.3'	1v16.78		1v16.23	C.2.0 / 28.0
C.3.5 / 27.0		1v16.75		C.1.0 / 24.3'

Sta	+	H.I.	-	Elev	Remks
		1v24.3v			
59+50					
60+00					
T.P.	4.43	1v22.10	6.65	1v17.67	
60+50					
61+00					
61+50					
62+00					
T.P.	3.28	1v15.78	9.60	1v12.50	
63+00					
64+00					
65+00					
T.P.	2.85	1v09.15	9.48	1v06.30	

South	℄ Elev.	North
	1v16.85	
C. 2.5 / 26.7'	1v16.67	C. 1.0 / 23.5
	1v16.19	
C. 0.5 / 22.7	1v15.42	C. 1.0 / 22.9
	1v14.35	
F. 1.0 / 21.5'	1v13.00	F. 0.5 / 21.3'
F. 1.0 / 20.7'	1v11.10	F. 1.0 / 20.3'
Gr. / 21.7'	1v09.20	F. 1.5 / 20.0'
Gr. / 22.3'	1v07.30	F. 1.0 / 20.7'

Sta	+	H.I.	-	Elev	Rem's	South	℄ Elev		North
		1209.15							
66+00						C.0.5 / 22.7'	1205.40		F.0.5 / 21.3'
67+00						C.0.5 / 23.0	1203.50		C.0.5 / 22.7'
+60							1202.36		
68+00						F.2.0 / 19.3'	1201.85		F.2.0 / 19.5
T.P.	5.47	1205.32	9.30	1199.85					
68+60							1201.71		
69+00	7' Berm on Both Sides					F.3.5 / 20.7'	1202.20		F.4.0 / 22.0
T.P.	9.83	1211.86	3.29	1202.03					
69+60							1203.56		
B.M.			2.32	1209.54					
70+0						C.1.0 / 23.9'	1204.80		F.0.5 / 20.0'
+50							1206.35		

Sta	+	H.I.	−	Elev.	Cen-S	South		℄ Elev.		North
B.M.	2.32	1x11.825		1x09.505						
71+00						C. 2.0 24.0		1x07.64		Gr. 22.3'
71+50								1x08.40		
72+00						C.0.5 22.5'		1x08.90		F.0.5 21.3'
73+0						F.0.5 21.3		1x09.90		F.1.5 20.3'
B.M	4.52	1x14.025		1x09.505						
74+0						C.0.5 23.0'		1x10.90		Gr. 21.9'
75+0						C.1.0 23.9'		1x11.90		Gr. 22.1'
T.P.	3.78	1x16.68	1.12	1x12.90						
76+0						F.0.5 20.9'		1x12.90		F.1.5 19.5
77+0						Gr. 26.3'	1213.75		1214.40	F.0.5 21.1'
77+25						C.0.5 27.7'	1x14.0		1x14.95	F.0.5 21.3

Sta	+	H I	-	Elev	Left
		1v16.68			
77+50					
T.P.	3.89	1v18.77	1.80	1v14.88	
77+75					
78+00		7' Berm on N Side			
T.P.	2.55	1v19.05	2.27	1v16.50	
78+14.90					
79+0				1v17.59	Used
B.M.	11.28	1v28.87	1.43	1v17.62	
79+40					
80+00					
T.P.	10.85	1v34.35	5.37	1v23.50	
81+00					
82+00					

South		& Elevation		North
C. 2.0 / 29.5'	1v14.35		1v15.38	F. 0.5 / 21.5'
C. 2.0 / 29.3'	1v14.50		1v15.63	Gr. / 21.5'
C. 1.0 / 26.9'	1v14.82		1v15.67	F. 3.0 / 21.3
F. 0.5 / 24.1	1v15.32		1v15.89	
F. 2.5 / 19.0'		1v18.00		C. 0.5 / 22.9'
		1v19.60		
C. 2.0 / 23.1'		1v22.00		C. 1.5 / 24.3'
C. 2.0 / 25.1'		1v25.75		C. 1.0 / 24.0'
F. 1.0 / 20.9'		1v29.00		C. 1.0 / 23.7'

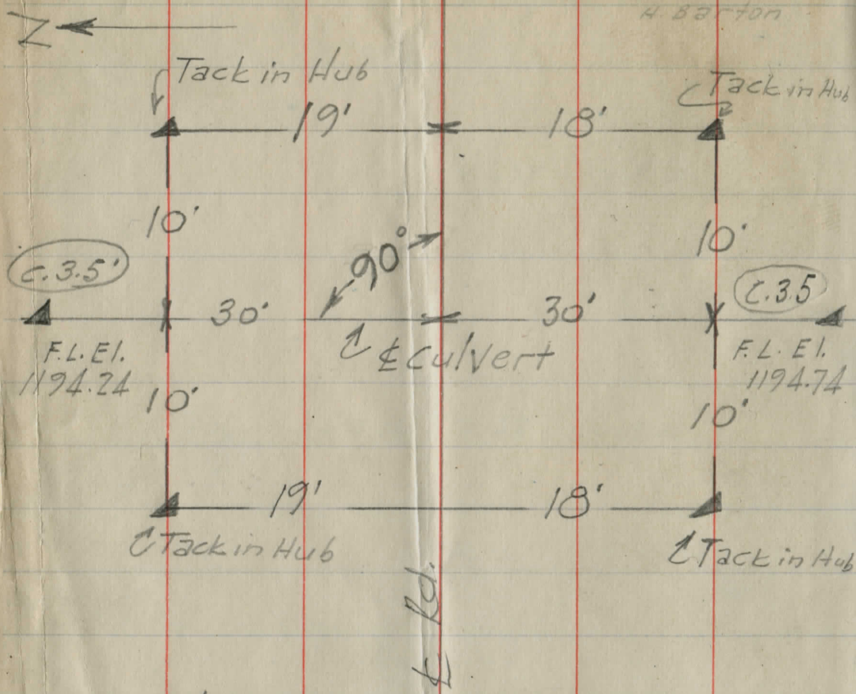
Sta	+	H.I.	−	Elev.	Remarks
		1234.35			
83+0					
T.P.	8.44	1240.94	1.85	1232.50	
84+0					
85+0	7.53	1243.53	4.94	1236.00	
86+00					
T.P.	8.91	1247.05	5.39	1238.14	
87+0					
B.M.			2.81	1244.25 Rec. 1244.24	
88+0	NOTE: Adjust slopes & ditches So as to Save Trees				
B.M.	2.71	1246.96		1244.25	
89+0					
T.P.	7.695	1253.61	1.045	1245.915	
90+0	Build "V" Type Ditch & Change Slopes on So. Side in order to Save Trees.				
T.P.	9.95	1261.95	1.61	1252.00	
91+0					
T.P.	11.39	1270.88	2.46	1259.49	

South	℄ Elevation	North
C. 2.0 / 25.5'	1232.00	C.0.5 / 22.9'
C. 2.0 / 24.7'	1234.94	Gr. / 22.3'
F.0.5 / 21.3'	1237.50	F.1.5 / 20.1'
F.1.0 / 20.3'	1240.14	F.2.0 / 19.5'
Gr. / 22.7'	1243.60	F.1.0 / 20.5'
C.1.0 / 23.5	1247.20	Gr. / 21.7
C.1.0 / 23.0	1251.64	F.1.0 / 20.9
C.3.5 / 27.0	1256.30	C.1.5 / 23.7
C.1.0 / 23.3'	1261.49	F.2.0 / 20.3'

Sta	+	H.I.	−	Elev.	Rem's
		1v70.88			
91+30					
B.M.			v.635	1v68.245	
92+0					
93+0					
T.P.	7.06	1v75.36	v.58	1v68.30	
94+0					
95+0					
96+0					
T.P.	6.56	1v79.46	v.46	1v72.90	
97+0					
98+0					
99+0					

Aug. 14, 1930 Wilson's Mills Rd.

S. Gold Jr.
S. Merritt
H. Barton



Sta 68+64 (Instead of 68+60 as shown on Plans)

4'x3' (Standard) Box Culvert

South	℄ Elevation	North
F. 1.5 / 19.5	1262.58	F.4.5 / 24.5'
F.2.5 / 21.1'	1264.80	F.3.5 / 21.3
Gr. / 21.0'	1267.80	C.0.5 / 23.1'
C.0.5 / 22.5'	1270.53	F.1.0 / 21.0'
Gr. / 21.9'	1271.60	F.1.0 / 21.1'
C.0.5 / 22.9'	1272.40	C.0.5 / 22.7'
C.0.5 / 22.5'	1273.20	F.1.0 / 21.0'
C.0.5 / 23.3'	1274.00	F.0.5 / 21.7'
C.0.5 / 22.7	1274.80	F.1.0 / 21.3

Sta	+	H.I.	-	Elev	Rem's
		1279.46			
100+0					
B.M.			4.12	1275.34	Nail Gone reading +.05 (BM)
100+50					
101+0					
T.P.	4.56	1280.66		1276.10	
102+0					
T.P.	3.89	1276.99	7.56	1273.10	
103+0					
T.P.	4.63	1275.13	6.49	1270.50	
104+0					
T.P.	7.64	1271.44	6.33	1268.80	
105+0					
106+0					
107+0					

South	℄ Elevation	North
C.0.5 23.5'	1275.60	F.0.5 21.5
C.0.5 23.1'	1275.70	Gr. 21.9'
C.1.0 23.7	1275.20	C.0.5 23.1
F.0.5 21.5	1273.60	Gr. 22.9'
F.1.5 20.5'	1272.00	F.1.5 20.1
F.0.5 21.5'	1270.40	
Gr. 22.0	1268.80	F.0.5 21.7'
C.0.5 22.5	1267.20	C.0.5 22.9'
C.1.5 24.5'	1265.18	Gr. 22.5'

Sta	+	H.I.	−	Elev.	Remks
		1271.44			
107+70					
T.P.	3.43	1264.73	10.14	1261.30	
108+0					
B.M			8.81	1255.92	1255.94 Rec'd
109+0					
B.M	2.24	1258.18		1255.94	
110+0					
111+0					
T.P.	3.60	1253.27	8.51	1249.67	
112+0					
T.P.	9.69	1256.09	6.87	1246.40	
113+0					
B.M.			2.11	1253.98	
114+0					
B.M.	1.70	1255.67		1253.97	
115+0					

South	℄ Elevation	North
	1263.28	
C.0.5 23.0'	1262.30	F. 1.0 21.9'
Gr 22.5	1258.58	F. 1.0 20.3'
F. 1.0 23.9'	1254.00	F. 0.5 25.5
F. 1.0 24.3'	1260.18	F. 0.5 24.9'
F. 2.0 22.7'	1248.70	F. 1.5 23.5'
F. 2.0 22.7'	1248.40	F. 2.0 23.1'
C. 0.5 25.5'	1248.10	F. 1.0 24.3'
C. 2.5 28.9'	1246.02	C. 2.5 29.0'

Sta	+	H.I.	−	Elev.	Rem's
		1255.67			
116+0					
117+0					

South	℄ Elevation	North
F.0.5 / 21.7'	1251.42	C.1.0 / 24.0'
F.0.5 / 21.5'	1252.60	GR / 22.0'

H. Patterson
M. Dorsa
G. Diedrich

Wilson Mills Rd
& Profile of Woodie Brook

7-9-62

BM	11.65	111.65		100.00
0+0			8.40	103.25
+50 W			6.76	104.89
1+00 W			5.19	105.46
+50 W			3.86	107.79
2+00 W			2.59	109.06
+50 W			1.35	110.30
3+00 W			0.33	111.32
BM	0.47	100.47		100.00
0+50 E			0.02	100.45
1+00 E			2.95	97.52
+50 E			5.80	94.67
2+00 E			7.77	92.70
+50 E			9.08	90.39
2+81 ± Cont.			9.71	90.76
3+00			9.75	90.72
+50			9.64	90.83
4+00			8.84	91.63
+50			9.20	91.27

Spk. N. Side Tel. Pole SE & Wilson Mills & Woodie Brook & Woodie Brook

		100.47		
5+00			10.30	90.17
+50			11.87	88.60
T.P.	3.51	92.13	11.85	88.62
6+00			5.30	86.83
+50			7.09	85.04
7+00			8.81	83.32
+50			10.60	81.53
T.P.	9.15	100.27	1.01	91.12
			0.27	100.00

BM	2.02	102.02		100.00	Spk. E. side Tel. Pole #60 3rd Pole S. of Thwing Rd.
0+0			5.40	96.62	100' S. of T.S.
+50			5.45	96.57	
1+00			5.48	96.54	T.S.
+50			5.20	96.82	
2+00			4.89	97.13	
+50			4.54	97.48	
3+00			4.29	97.73	

		102.02		
3+50			4.45	97.57
4+00			5.24	96.78
+50			6.10	95.92
5+00			6.52	95.50
+50			7.15	94.87
6+00			7.54	94.48
+50			8.30	93.72
7+00			8.55	93.47 ✓
+50			8.26	93.76
8+00			7.90	94.12
+50			7.89	94.13
9+00			7.35	94.67
+50			6.65	95.37
10+00			6.18	95.84
T.P. +50	7.42	103.19	6.25	95.77
11+00			7.60	95.59
+50			7.75	95.44
12+00			8.05	95.14
+50			8.25	94.94

10+10
= C.S. N. end.

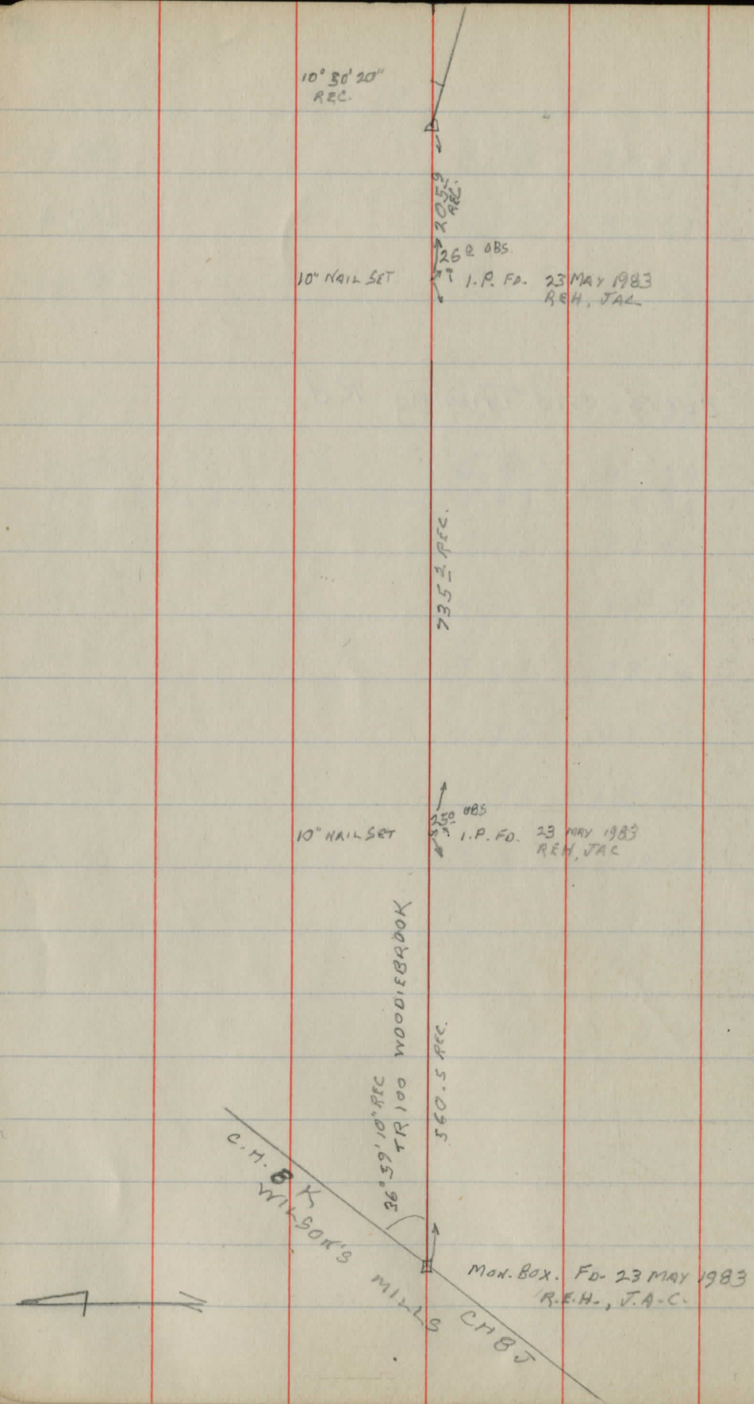
	103.19		
13+00		B.70	94.49
+50		9.50	93.69
14+00		10.25	92.94
0+0		9.47	93.72
+50		6.80	96.39
+66 I Pin E Wilson Mills & Thwing		5.43	97.76
1+00		4.78	98.41
+50		4.50	98.69
2+00		3.43	99.76
+50		2.25	100.94
3+00		0.98	102.21
B.M.		3.21	99.98

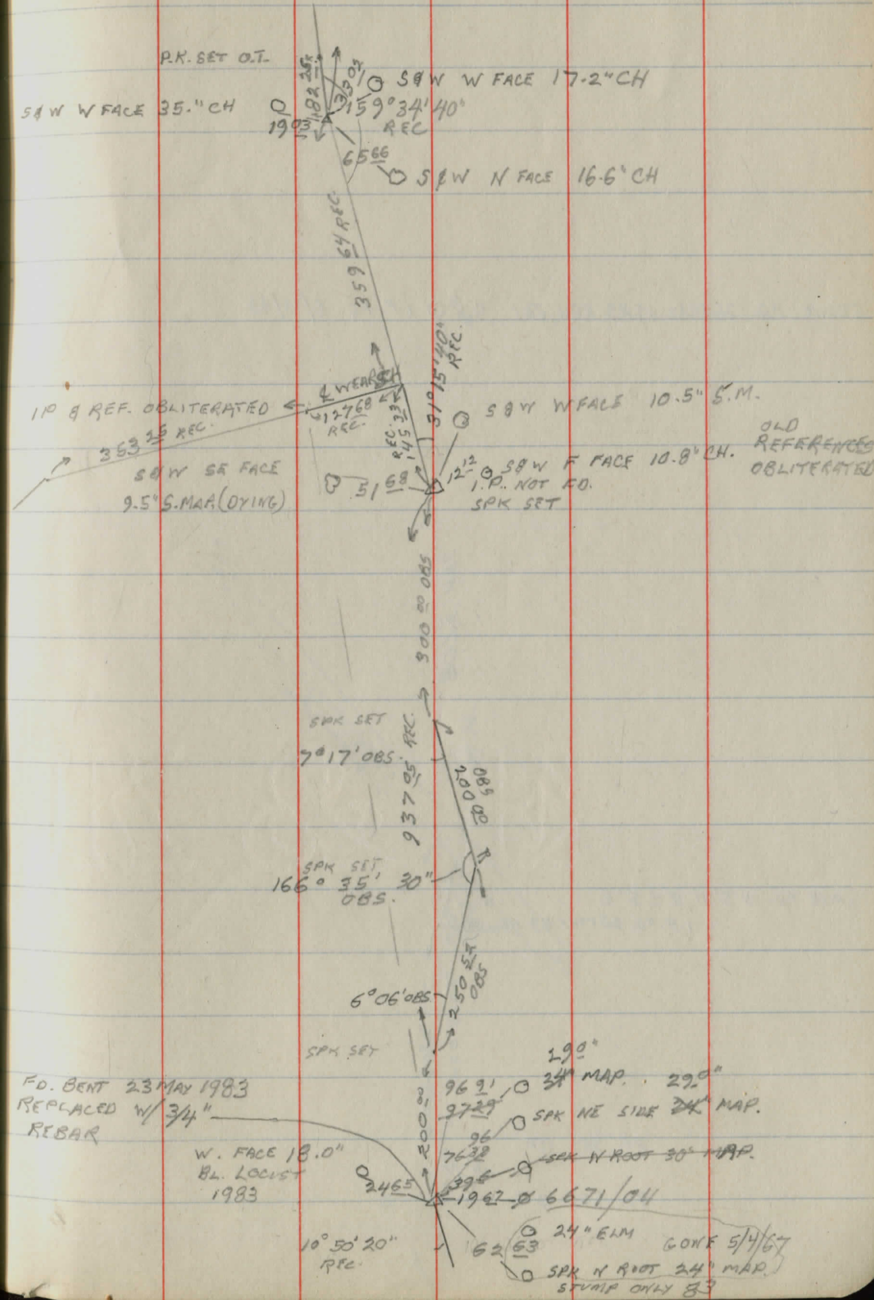
New ℄ curve and Thwing Rd.

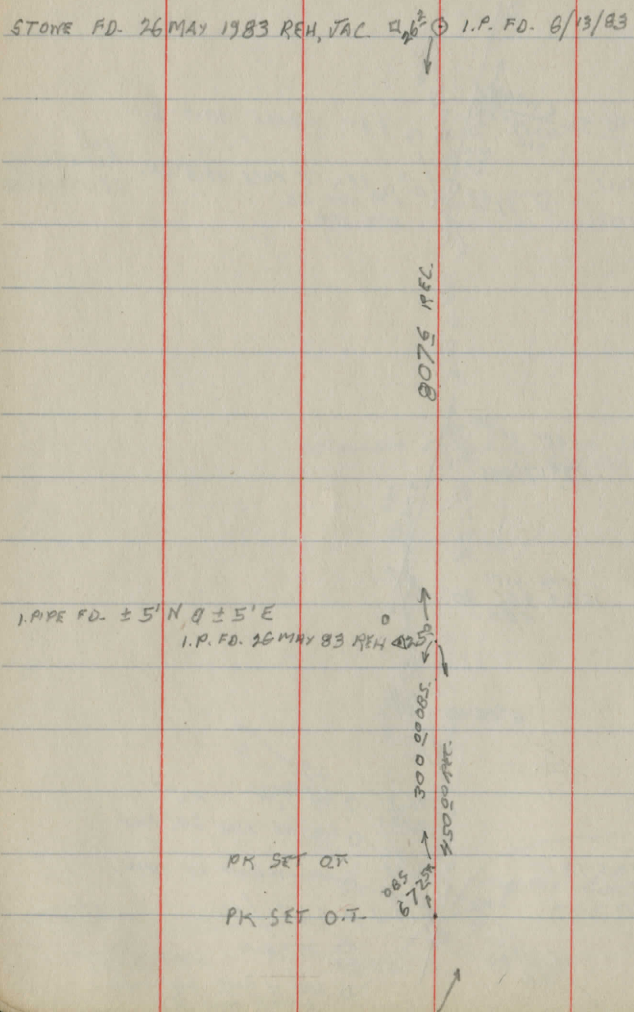
R.E. HERSHBERGER
J.A. CHOLLEY
G.A. MOHNACSKY
D.W. SEWELL

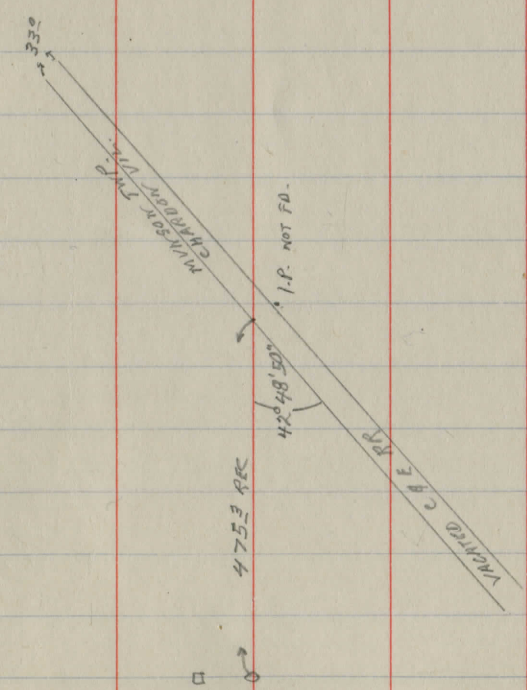
TR 100 WOODIEBROOK

23 MAY - 14 JUNE 1983
MILD






STONE FD. 26 MAY 1983 REH, JAC.
26
I.P. FD. 6/13/83
8076 REC.
I. PIPE FD. ± 5' N & ± 5' E
I.P. FD. 26 MAY 83 REH
25
300.00 OBS.
4500.00 REC.
PK SET O.T.
OBS
6725
PK SET O.T.


33
MUNSON TWP.
CHARDON VIL.
I.P. NOT FD.
42°48'50"
4753 REC
VACATED C & E RR

Sta	+	H.I.	−	Elev	Rem's
B.M.	0.0	1253.96		1253.96	
N.F.L.			9.43	1244.53	
S." "			9.89	1244.07	
0+50			9.06	1244.90	1st Stake
1+00			9.09	1244.87	
1+50			9.60	1244.36	
2+00			10.88	1243.08	
2+50			11.55	1242.41	
3+00			10.76	1243.20	
3+50			11.05	1242.91	
4+00			11.02	1242.94	
4+50			11.90	1242.06	

Gr. W. Ditch

1244.53	
1244.07	
1243.84	C.6.0
1243.62	C.5.5
1243.39	C.5.0
1243.17	C.4.5
1242.94	C.4.5
1242.72	C.4.0
1242.49	C.4.0
1242.25	C.3.5
1242.02	

B.M. 1255.99
+ 0.98
1256.97
- 8.05
T.P. 1248.92
+ 6.09
H.I. 1255.01

1256.42
- 2.415
1254.005

1254.105
2.415
1256.520

T.P 1248.92
+ 7.500
1256420
2.415
1254.005

B.M. 1253.965
+ 5.310
H.I. 1259.275
- 2.865
T.P. 1256.410
+8.52
H.I. 1264.930
- 2.90
T.P. 1262.030
10 320
H.I. 1272.350
0 0.15
1272335

1268 325
1268.185
002.140

1261.72
5.53
1256.19

1253.965
2.765
1256.730
1255.99
74

56.205
2.11
54.095

1256.87

1256.87
2.765
1254.105
1253.965
140

1256.87
0.645
1256.225

1254.105
2.765
1256.870
0.645
1256.225
1255.99
(23)

1256.87
2.77
1254.10
1253.965
0.135

DISTANCES FROM CENTER FOR ROADWAY CROSS-SECTIONING.

ROADWAY [illegible] SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.
R.